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COMBINING IN SITU RECOVERY AND ION EXCHANGE AT THE KAPUNDA COPPER PROJECT

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ISR AND ION EXCHANGE

- IX is well-suited for recovery of low- to moderate-concentrations of value metals from complex processing liquors. Very-well matched to PLS processing / lixiviant return.
- ISR has a different cost structure to drill-blast-haul-mill-etc. Not reliant on bigger-is-better for payback.
- Ion exchange suits incremental / modular development
- Uranium – 50% global supply
- Copper – Taseko's Florence ISR
- Nickel – KazNickel's Gornostayevskoye
- Future: Rare earths; other battery minerals; gold (paleochannel deposits)

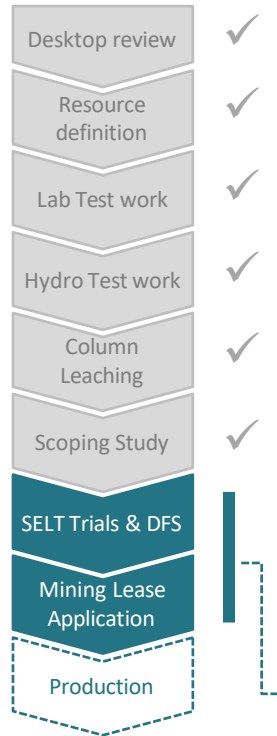


Gornostayevskoye – Nickel ISR
IX



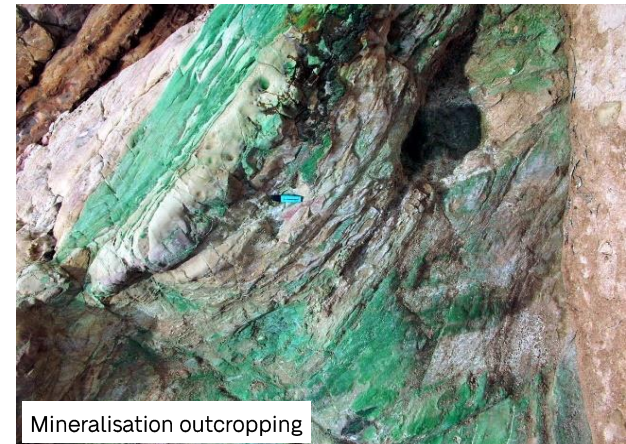
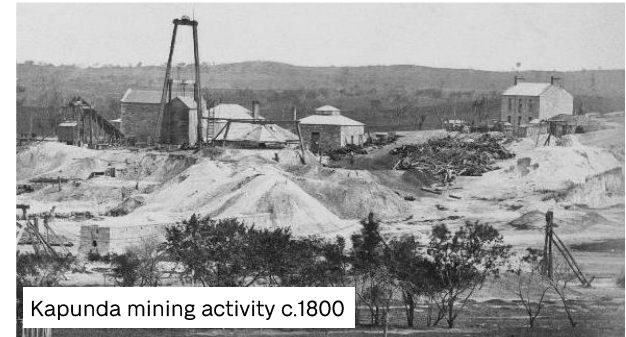
South Inkai – Uranium ISR IX

KAPUNDA PROJECT OVERVIEW

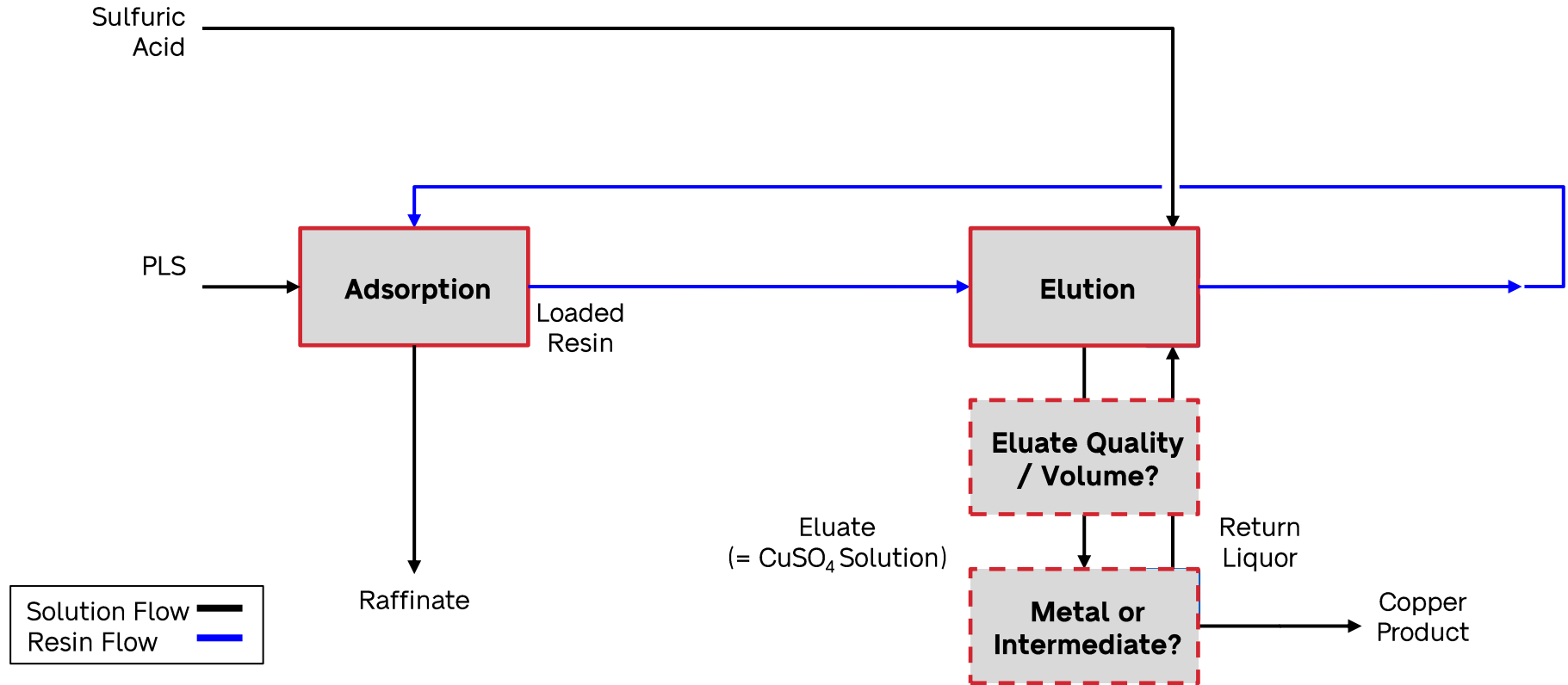


Interest	ECL has earned 50% project interest and is earning to 75%
Location	150 km north of Adelaide, South Australia
Infrastructure	Proximity to power, water and workforce
Resource	JORC resource 102MT @ 0.23% Cu, signif. gold upside potential
Geology	Siltstone, fracture fill mineralisation
Social	Built strong research based community support for project
ISR Characteristics	<ul style="list-style-type: none"> - Depth of mineralization (40-250m) - Visible core is highly weathered and fractured, likely to be permeable - Mineralisation sits under water table, right hydrogeological environment - Copper already present in water monitoring bores (suggesting readily leachable)

Kapunda is a near term copper/gold ISR project ready for definitive feasibility and mining lease application



CONCEPTUAL RECOVERY FLOWSHEET



PLS + COPPER EXTRACTION (ADSORPTION)

- Feed liquor

	Al	Co	Cu	Mn	Ni	Zn	Fe	ORP (Ag/AgCl)	pH
Feed, mg/L	82	6	1040	6	9	54	1810	341	2.76

- Preparatory batch testwork
- Fe^{2+} as major impurity, Cu-to-Fe ratio of 0.6
- pH and Fe^{2+} suppressed Cu loading; but Cu^{2+} can displace Fe^{2+}
- Partial oxidation of Fe^{2+} to Fe^{3+} during contact
- Subsequent countercurrent extraction campaign to generate bulk loaded resin



ADSORPTION – MINI-PILOT

- Loaded resin shows upgrade and purification:

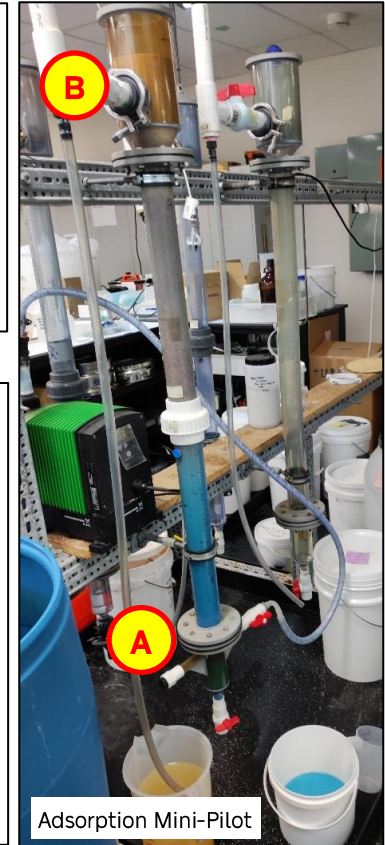
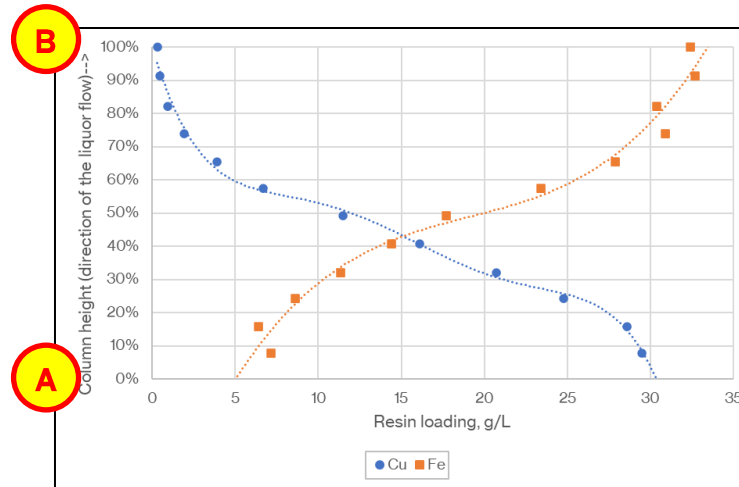
	Al	Co	Cu	Mn	Ni	Zn	Fe	pH
Resin, g/L	1.3	0.1	29.4	~0	0.3	1.4	7.6	2.7

Feed Cu-to-Fe = 0.6

Loaded Resin Cu-to-Fe = 3.9

- Some oxidation of Fe^{2+} to Fe^{3+} ; some solids formation
- Trade-off exists on resin residence time/ solution contact time / Cu slip to raffinate
- Cu extraction prioritised

Column resin volume	2 L
Solution flowrate	~ 3 BV/h
Solution-to-resin flowrate	~ 33
Cu extraction	~100%
Iron rejection	>90%
Resin loaded	5.7L



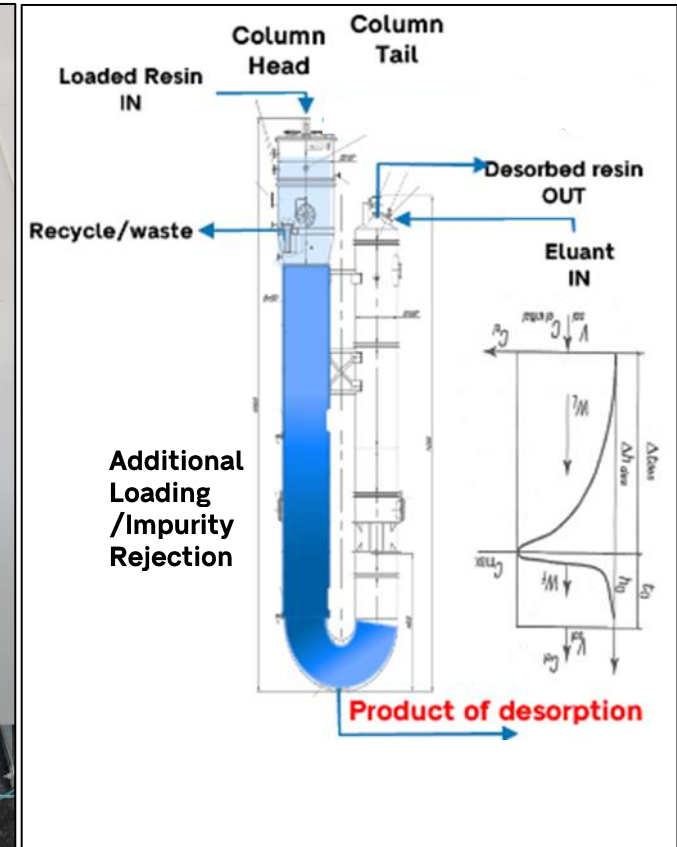
ELUTION – MINI-PILOT

- Counter-current movement of solution and ion exchange resin in U-shaped column
- Further upgrade and purification of Cu

	Al	Cu	Mn	Zn	Fe
Feed, mg/L	82	1040	6	54	1810
Resin, g/L	1.3	29.4	~0	1.4	7.6
Eluate, g/L	<0.1	87.1	<0.1	<0.1	5.6
Department %	0	100	0	0	25

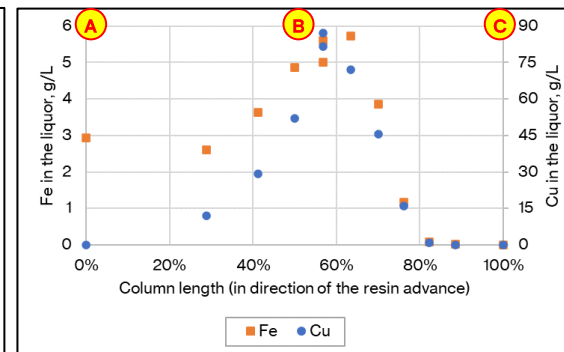
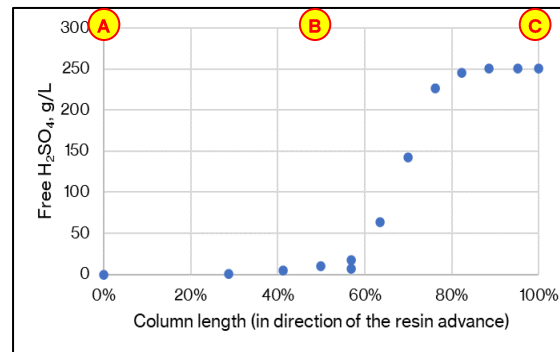
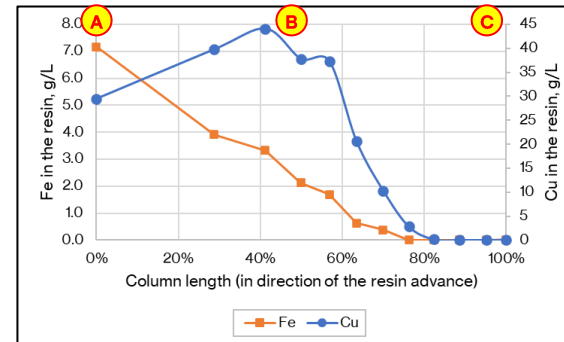
- Stoichiometric reagent consumption

Resin processed	~5.7 L
Eluant H_2SO_4 conc.	~250 g/L
Eluant-to-resin flowrate	0.61
Eluate generated	~1 L
Eluate-to-resin flowrate	0.34



ELUTION – MINI-PILOT

- Fe^{2+} scrubbing (A \rightarrow B)
- Scrubbing accomplished with 80-90 g/L Cu solution in the presence of ~5 g/L Fe and <10 g/L H_2SO_4
- Cu loading increases 30 to 45 g/L (A \rightarrow B)
- Fe loading decreases 7.6 to ~2 g/L (A \rightarrow B)
- Remaining 2 g/L as Fe^{3+}
- Residual Cu and Fe loading <0.05 g/L (at C)



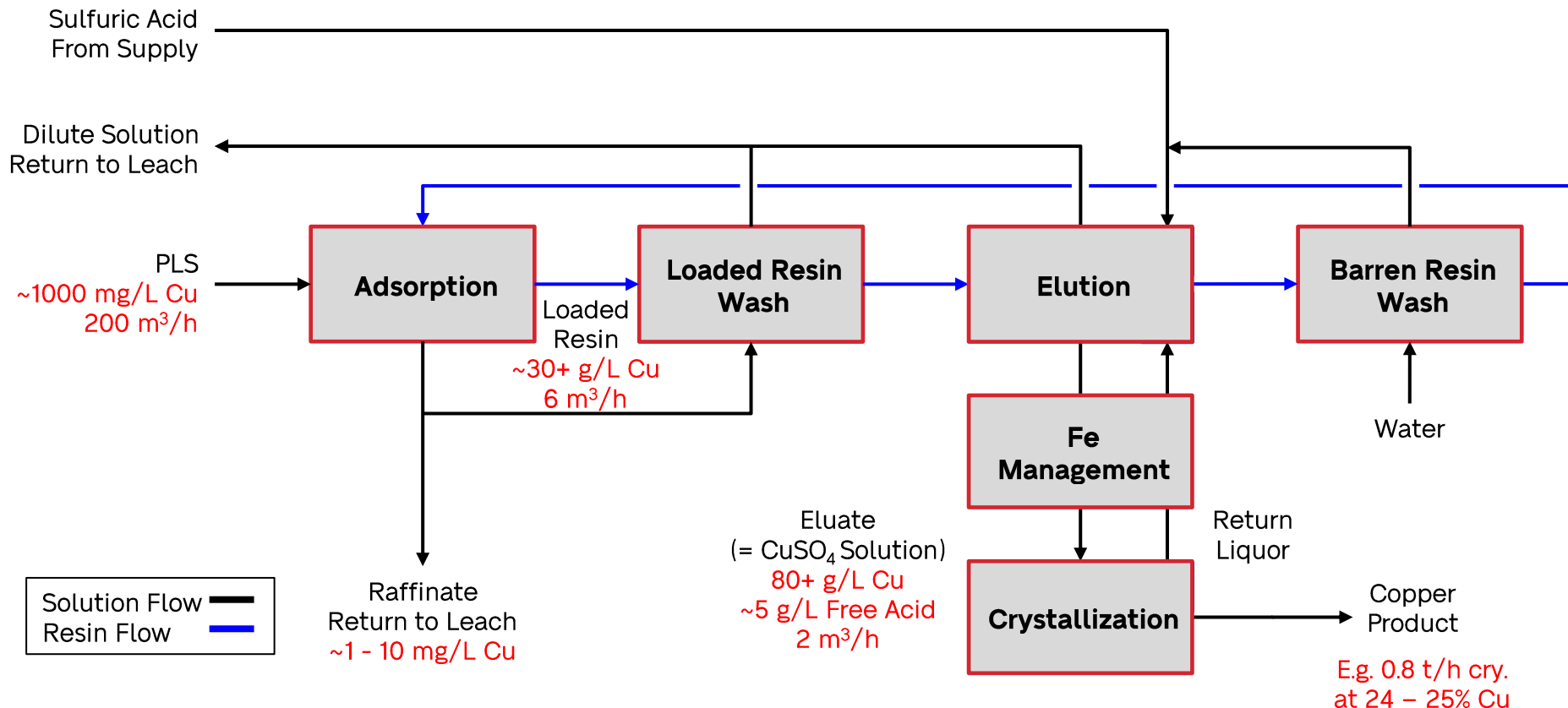
CRYSTALLISATION - BENCHSCALE

- Eluate homogenised and batch processed
- Volume reduction to saturation point at 75°C, targeting controlled crystallisation of $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$
- Under controlled crystallisation, a difference in Cu- and Fe-sulfate crystallisation leads to further Cu purification
- Technical grade product spec. reached without any eluate pre-treatment (e.g. neutralisation or hydrolysis)

	Al	Co	Cu	Mn	Ni	Zn	Fe	Cu/Fe
Feed, mg/L	82	6	1040	6	9	54	1810	0.6
Resin, g/L	1.3	0.1	29.4	~0	0.3	1.4	7.6	4
Eluate, g/L	<0.1	<0.1	87.1	<0.1	0.3	<0.1	5.6	16
$\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$ crystals, mg/kg	<25	<10	249000	<4	26	9	1723	144
Technical grade spec $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$, mg/kg			247000				3000	82



COMMERCIAL-SCALE FLOWSHEET



CAPITAL COST ESTIMATE (CLASS 4)

- 3 trains * 200 m³/h PLS; centralised crystallisation
- 5,000 tpa Cu equivalent ~ 20kt crystal
- Process flow diagram developed to identify key process plant equipment items (from PLS through to raffinate + bagged product)
- Major equipment prices assessed based on material off-take estimates or factored from prior projects
- Parametric method for other components (e.g. factors from in-house database; Lang factors etc.)
- Resulting capital intensity ~\$7000/tpa Cu

Direct Costs	US\$ M
Purchased equipment cost	12.4
Installation	5.0
Civils	1.9
Utilities / services upgrade, tie-in	0.6
Total direct costs	19.9
Indirect Costs	US\$ M
Engineering and supervision	2.2
Construction common distributables	1.4
Freight (inc. packaging)	0.6
Total indirect costs	4.2
First Fill	US\$ M
Reagents + Resin	10.6
TOTAL INSTALLED COST	34.7

- ISR + IX
 - Modular IX configuration for satellite or phased development
 - Further optimisation opportunities exist due to the PLS/Raffinate exchange between ISR and IX
- Impurity Management
 - Pre-treatment of PLS (e.g. pH, Eh adjustment) unnecessary, in this case
 - Solids formation (gypsum, metal hydroxides) manageable with moving bed ion exchange column
 - Given the scrubbing achieved in elution, Fe(III) is the main impurity to manage in eluate
- Product Formation
 - Moving-bed ion exchange provides a path from PLS to technical-grade product at Kapunda
 - Concentrated, (partially) purified liquor creates product formation options inc. technical grade salt, metal precipitates, cathode.
 - Driven by project location, market considerations (volume, payability), infrastructure, etc.



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